

Claims

1. A motor vehicle air conditioning unit, provided  
5 with a supercritical refrigerant circuit (10)  
comprising a compressor (14), a gas cooler (11), an  
expander (12), defining a refrigerant flow area, and an  
evaporator (13), the assembly further including an  
10 electronic control device designed to interact with the  
refrigerant circuit,  
characterized in that the electronic control device  
includes a calculating function using an estimate of  
the flow area of the expander, the density ( $\rho$ ) of the  
15 refrigerant and the pressure ( $P_{20}$ ) of the refrigerant at  
the inlet of the expander in order to calculate an  
estimate of the refrigerant mass flow rate ( $m_{exp}$ ) at the  
expander.

2. The air conditioning unit as claimed in claim 1,  
20 characterized in that the flow area of the expander is  
estimated from the value of the refrigerant pressure  
( $P_{20}$ ) at the inlet of the expander.

3. The air conditioning unit as claimed in claim 2,  
25 characterized in that the electronic control device is  
capable of reacting to the fact that the value of the  
refrigerant pressure  $P_{20}$  at the inlet of the expander  
is:

. less than or equal to a first pressure value  
30  $P_1$ , a first constant  $S_1$  being assigned to the flow area  
 $S$  of the expander;

. less than or equal to a second pressure value  
 $P_2$  greater than the first pressure value  $P_1$ , by solving  
the following equation in order to calculate an  
35 estimate of the flow area  $S$  of the expander:

$$S = S_1 + (S_2 - S_1) \times (P_{20} - P_1) / (P_2 - P_1),$$

where  $S_2$  is a second constant;

. less than or equal to a third pressure value  $P_3$

. less than or equal to a third pressure value  $P_3$  and greater than the second pressure value  $P_2$ , solving the following equation in order to calculate an estimate of the flow area  $S$  of the expander:

5           
$$S = S_2 + (S_3 - S_2) \times (P_{20} - P_2) / (P_3 - P_2),$$
  
          where  $S_3$  is a third constant; and

. greater than or equal to the third pressure value  $P_3$ , a fourth constant  $S_4$  being assigned to the flow area of the expander.

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4. The air conditioning unit as claimed in claim 3, characterized in that the first pressure value  $P_1$  is approximately equal to 80 bar, the second pressure value  $P_2$  is approximately equal to 110 bar and the  
15 third pressure value  $P_3$  is approximately equal to 135 bar and in that the first constant  $S_1$  is approximately equal to  $0.07 \text{ mm}^2$ , the second constant  $S_2$  is approximately equal to  $0.5 \text{ mm}^2$ , the third constant  $S_3$  is approximately equal to  $0.78 \text{ mm}^2$  and the fourth constant  
20  $S_4$  is approximately equal to  $3.14 \text{ mm}^2$ .

5. The air conditioning unit as claimed in one of the preceding claims, characterized in that the calculating function is specific to calculating the density ( $\rho$ ) of  
25 the refrigerant from the refrigerant temperature ( $T_{30}$ ) at the inlet of the expander and from the refrigerant pressure ( $P_{20}$ ) at the inlet of the expander.

6. The air conditioning unit as claimed in claim 5,  
30 characterized in that it includes a probe (30) placed at the inlet of the expander (12) for measuring the refrigerant temperature ( $T_{30}$ ) at the inlet of the expander.

7. The air conditioning unit as claimed in one of the preceding claims, characterized in that it includes a  
35 sensor (20) placed at the inlet of the expander (12)

for measuring the refrigerant pressure ( $P_{20}$ ) at the inlet of the expander.

8. The air conditioning unit as claimed in one of the preceding claims, characterized in that the electronic control device further includes a power estimation function capable of estimating the power absorbed by the compressor from:

- the refrigerant mass flow rate ( $m_{exp}$ ) provided by the calculating function;
- the work ( $\Delta H_{ise}$ ) of the compressor; and
- the rotation speed ( $N$ ) of the compressor.

9. The air conditioning unit as claimed in claim 8, characterized in that the electronic control device is capable of estimating the work ( $\Delta H_{ise}$ ) of the compressor from the refrigerant pressure ( $P_{20}$ ) at the inlet of the expander, from the refrigerant pressure ( $P_{35}$ ) at the inlet of the compressor and from a refrigerant temperature ( $T_{comp}$ ) relative to the compressor.

10. The air conditioning unit as claimed in claim 9, characterized in that the refrigerant pressure ( $P_{35}$ ) at the inlet of the compressor is estimated from a pressure ( $P_{50}$ ) at the inlet or at the outlet of the evaporator (13) combined with the refrigerant mass flow rate ( $m_{exp}$ ).

11. The air conditioning unit as claimed in claim 10, characterized in that the pressure ( $P_{50}$ ) at the inlet or at the outlet of the evaporator (13) is determined from the refrigerant temperature ( $T_{50}$ ) at the inlet or at the outlet of the evaporator (13), said temperature being either measured by a probe or estimated from:

- a temperature ( $T_{40}$ ) relative to the evaporator (13);

- the efficiency ( $\eta_{\text{evap}}$ ) of the evaporator (13);
- and
- the temperature ( $T_{60}$ ) of the air to be cooled.

5 12. The air conditioning unit as claimed in one of  
claims 9 to 11, characterized in that the refrigerant  
temperature relative to the compressor (10) is the  
refrigerant temperature ( $T_{35}$ ) at the inlet of the  
compressor.

10 13. The air conditioning unit as claimed in claim 12,  
characterized in that it includes a probe (35) placed  
at the inlet of the compressor (14) for measuring the  
refrigerant temperature ( $T_{35}$ ) at the inlet of the  
15 compressor.

14. The air conditioning unit as claimed in one of  
claims 9 to 11, characterized in that the refrigerant  
temperature relative to the compressor (14) is the  
20 refrigerant temperature ( $T_{36}$ ) at the outlet of the  
compressor.

15. The air conditioning unit as claimed in claim 14,  
characterized in that it includes a probe (36) placed  
25 at the outlet of the compressor (14) for measuring the  
refrigerant temperature ( $T_{36}$ ) at the outlet of the  
compressor.